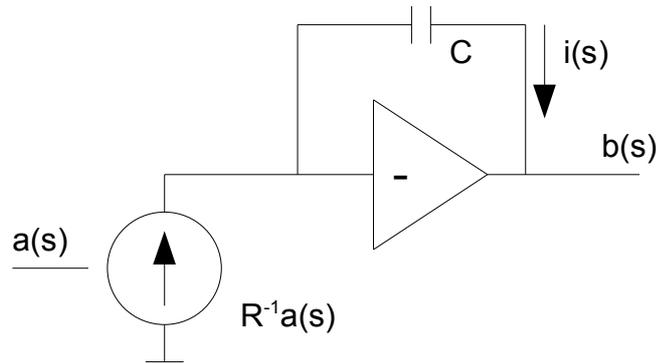


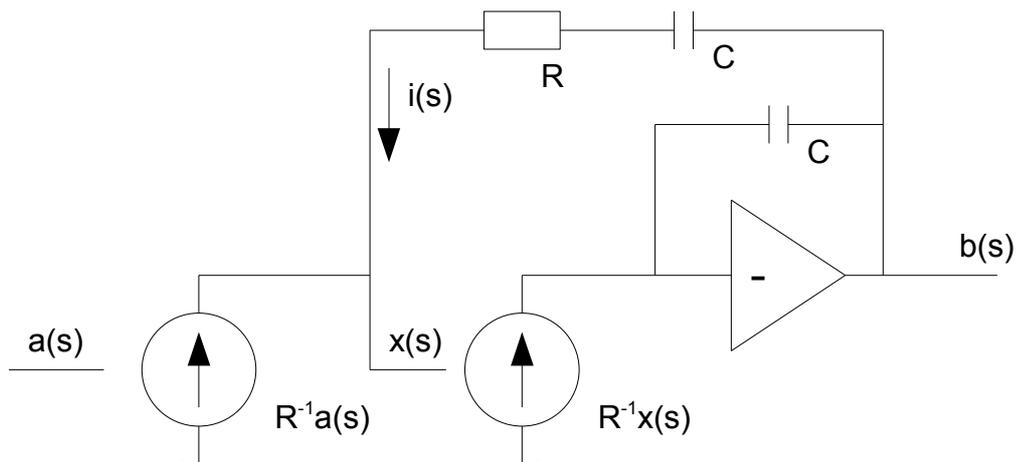
Integrator (VAS) with preceding transconductance stage



$$b(s) = -x_c(s)i(s) = -\frac{1}{sC}i(s) = -\frac{1}{sRC}a(s)$$

$$G(s) = \frac{b(s)}{a(s)} = -\frac{1}{sRC}$$

Additional Miller compensation loop with matched zero



$$b(s) = -\frac{1}{sRC}x(s)$$

$$i(s) = \frac{b(s) - x(s)}{R + (sC)^{-1}} = sC \frac{b(s)(1 + sRC)}{1 + sRC} = sCb(s)$$

$$a(s) = -Ri(s) = -sRCb(s)$$

$$G(s) = \frac{b(s)}{a(s)} = -\frac{1}{sRC}$$

The new transfer function is of first order, if all elements are perfectly matched. The closed-loop transfer function of the „inner“ loop remains first-order, since the impedance at $x(s)$ is theoretically infinity. Thus, the series of R and C does not influence its $G(s)$. The trick with the voltage divider (see matzes-amp.pdf in post #1) helps to translate that to reality.